

QUENCH-11 test Quench Phase

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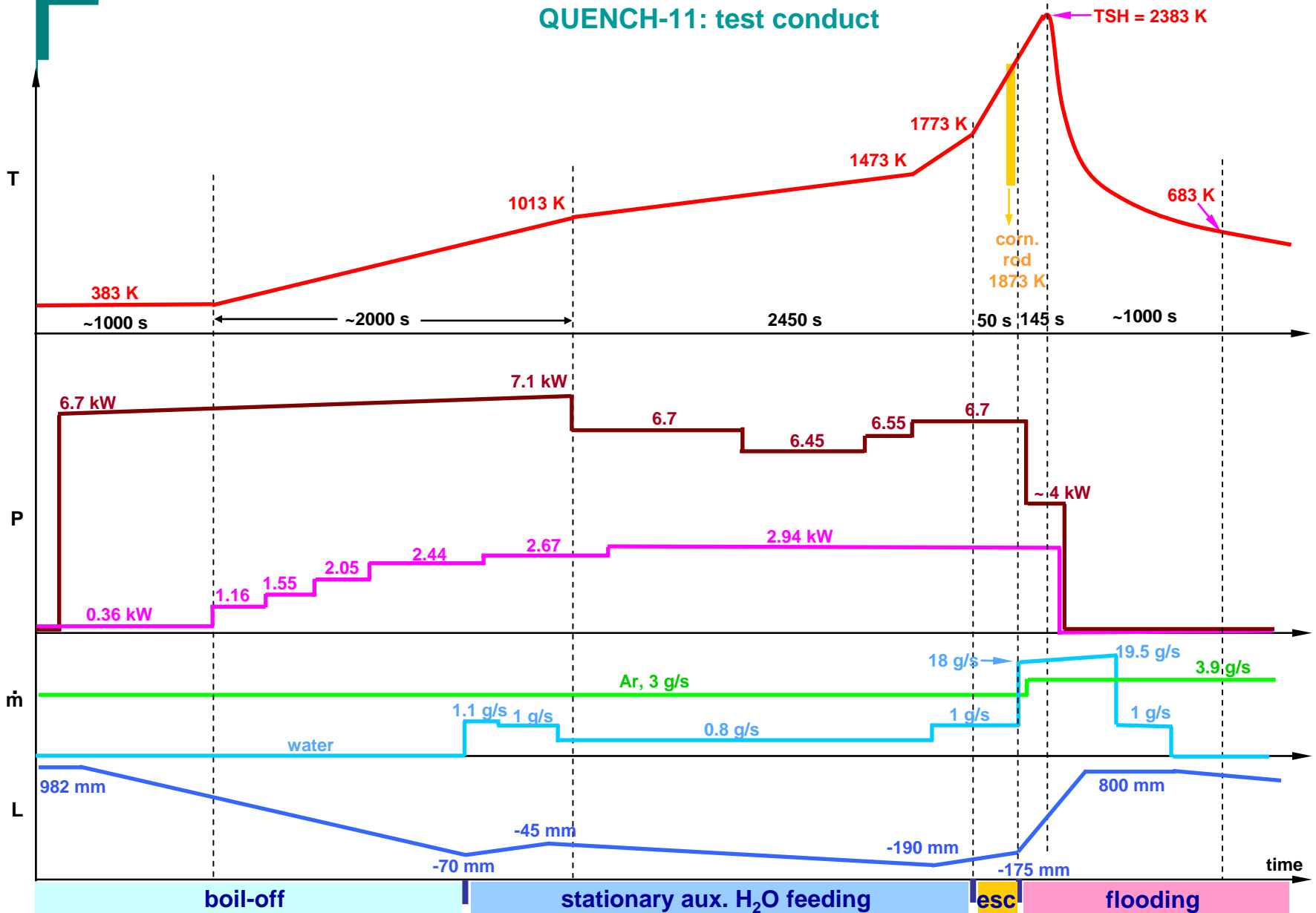


Objectives of the QUENCH-11 test

- simulation of a depressurised plant sequence in which the core would be essentially dried-out
- limited steam flow due to boiling of residual water
- simulation of reflood situations with a low mass flow rate

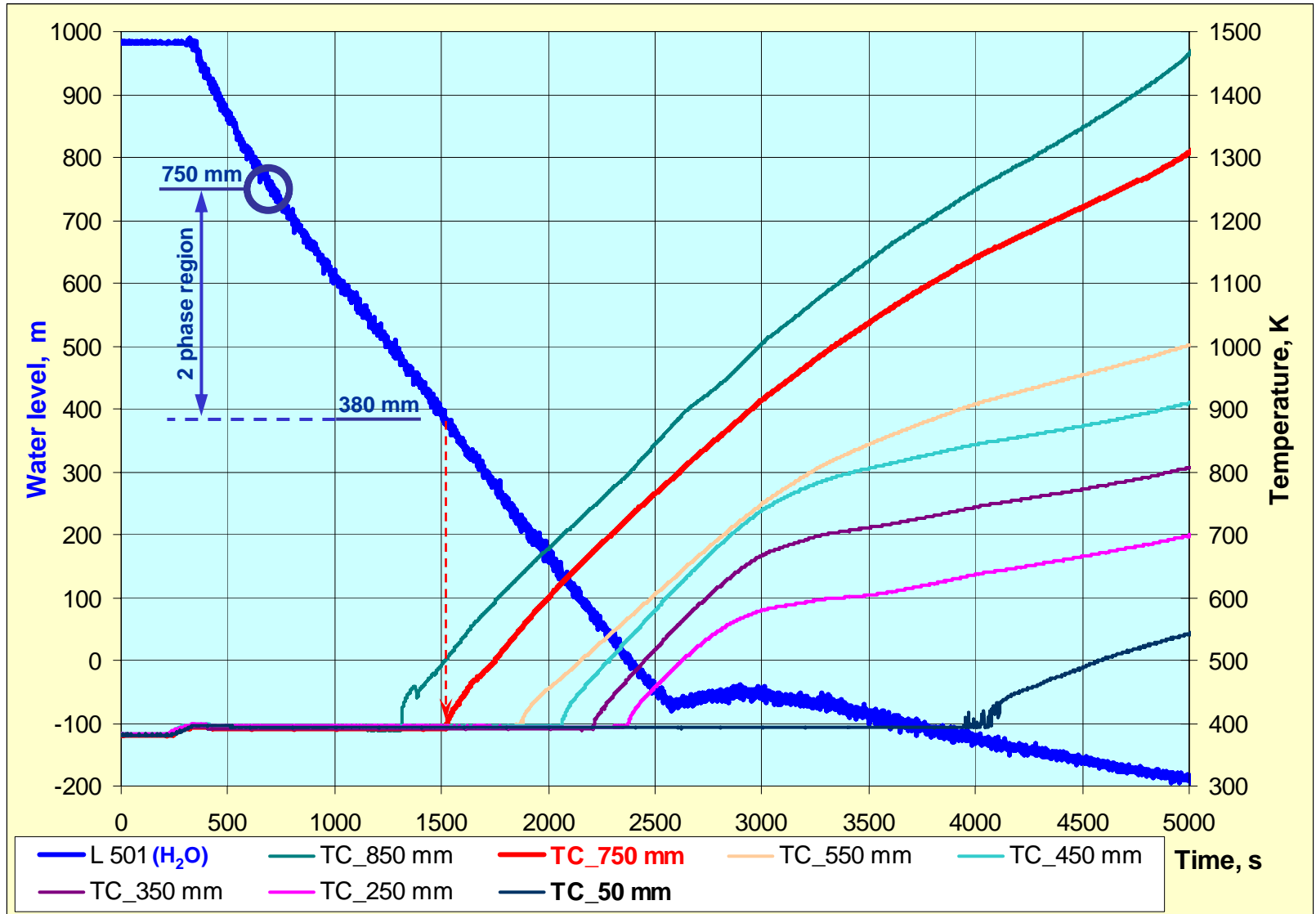


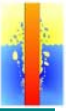
QUENCH-11: test conduct



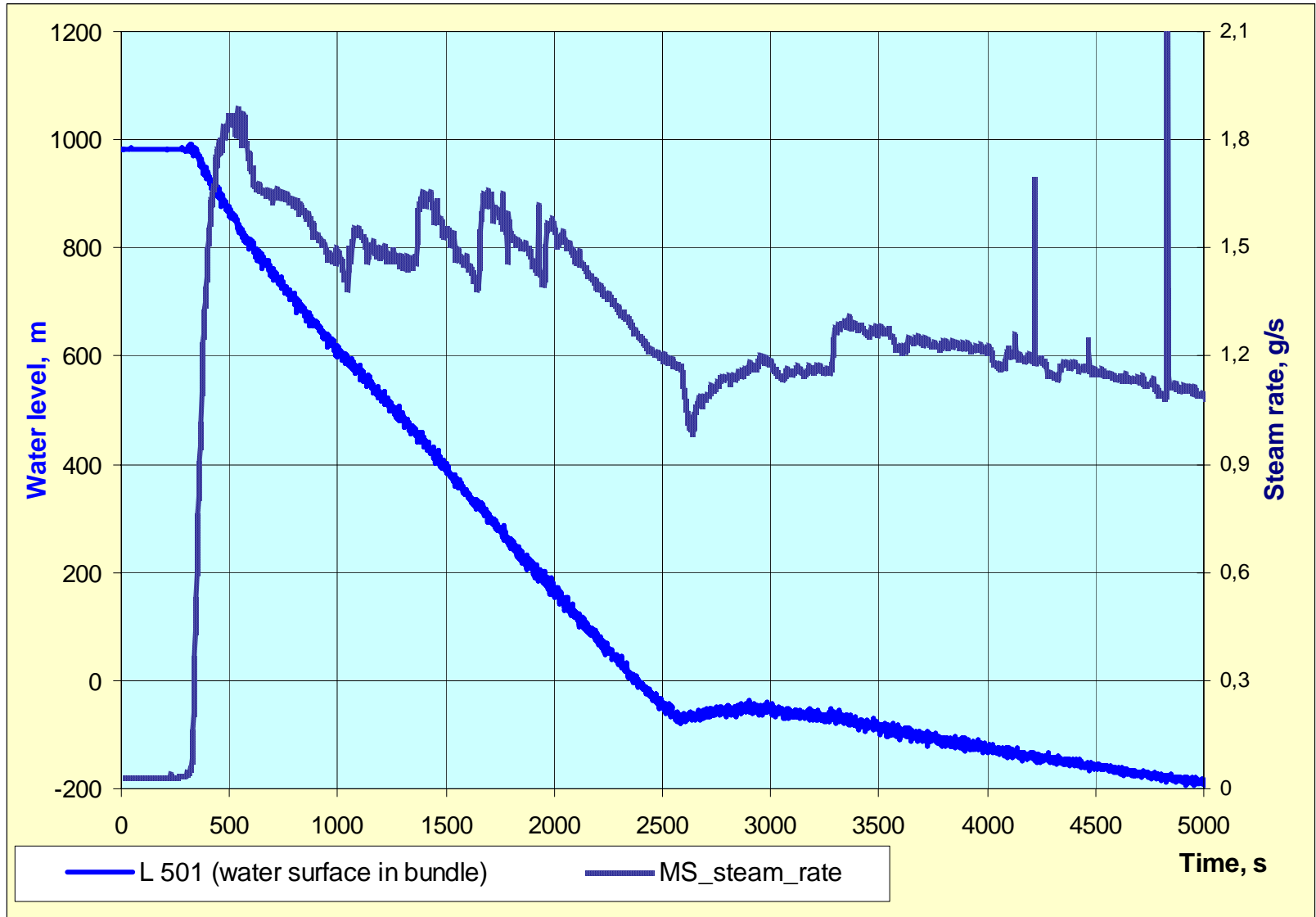


QUENCH-11, boil-off phase: delayed TC reaction on the falling water surface
due to two-phase region above the water surface.



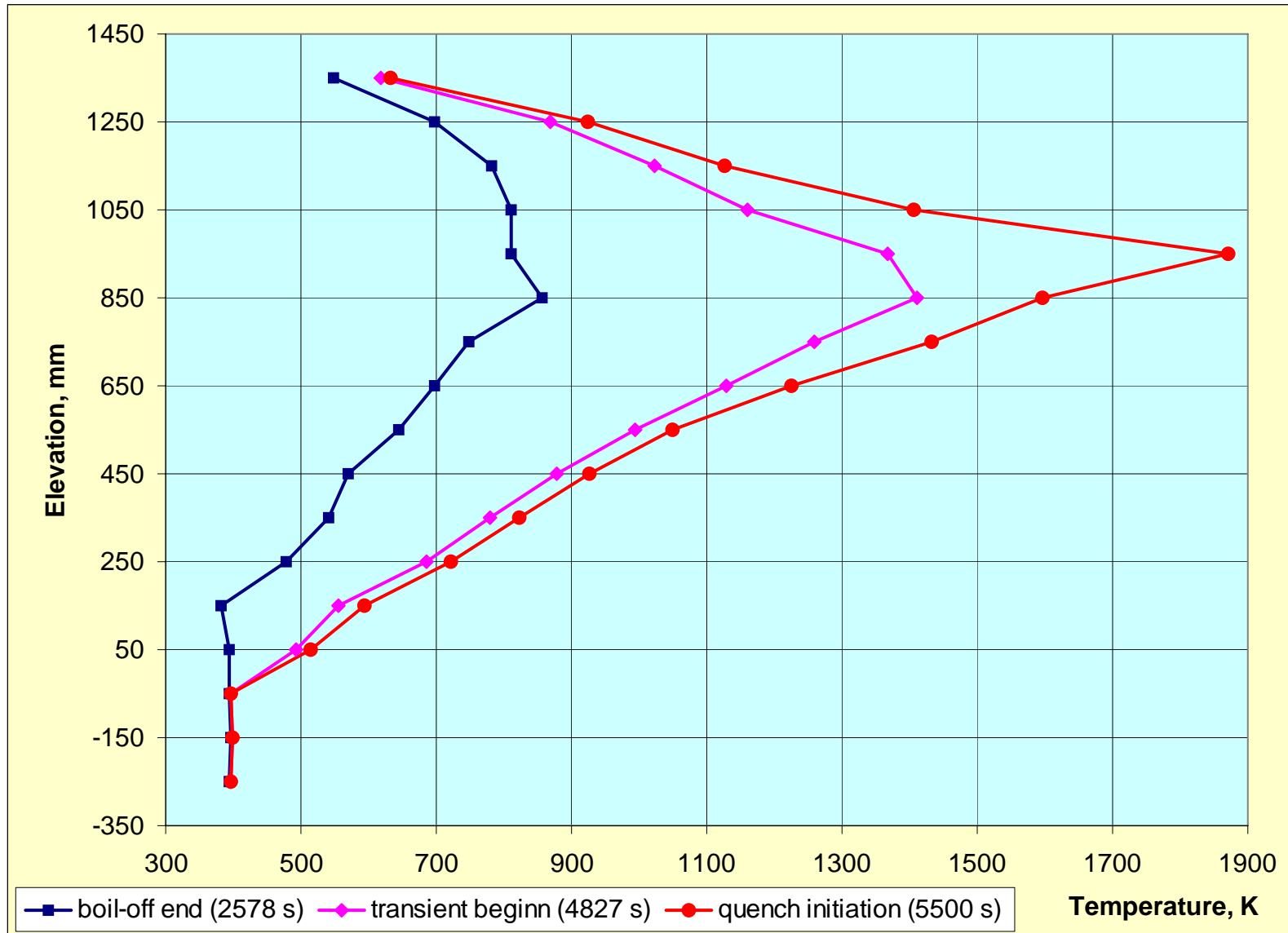


QUENCH-11, boil-off phase: steam generation due to evaporation



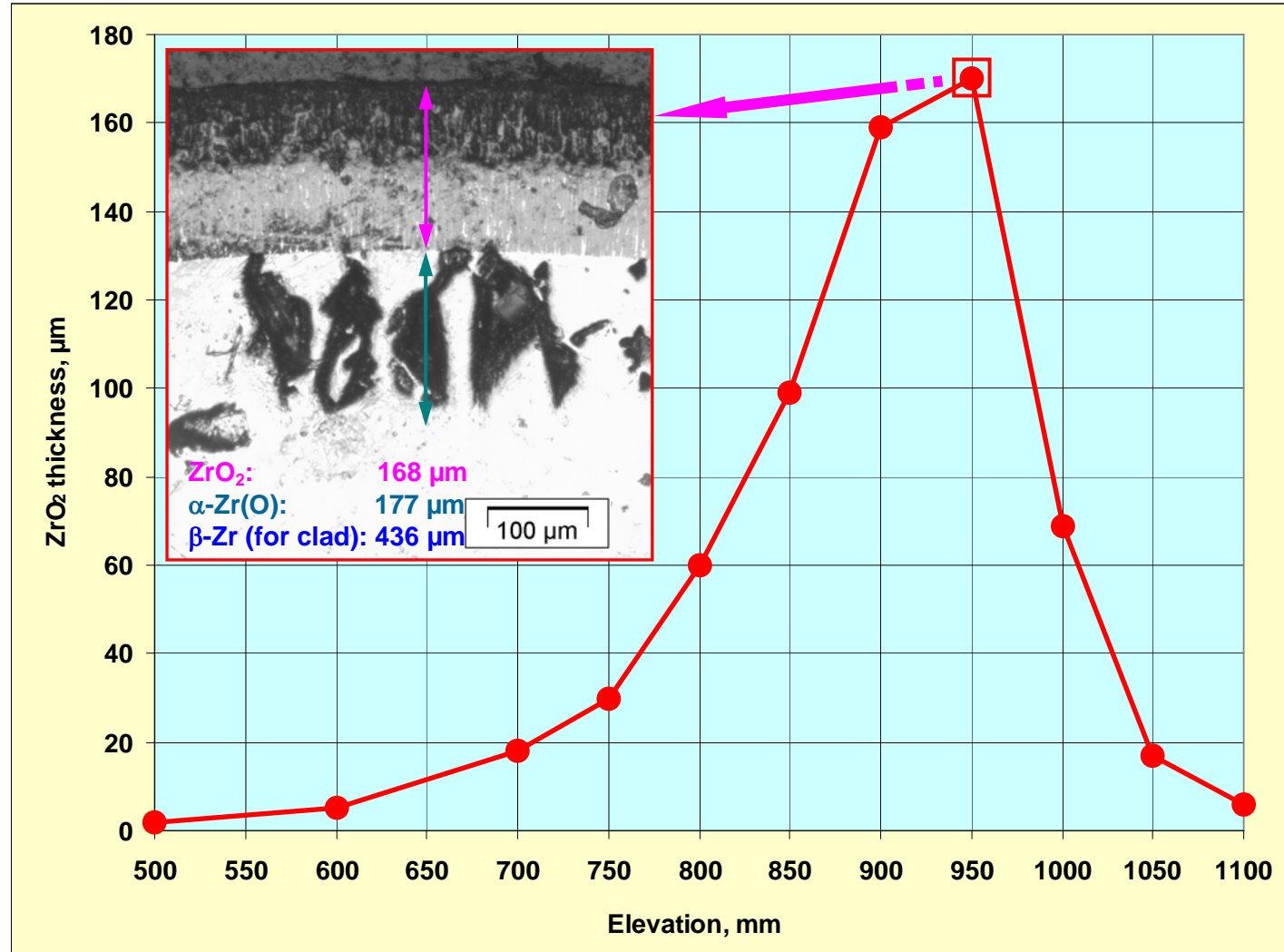


QUENCH-11: axial temperature profiles



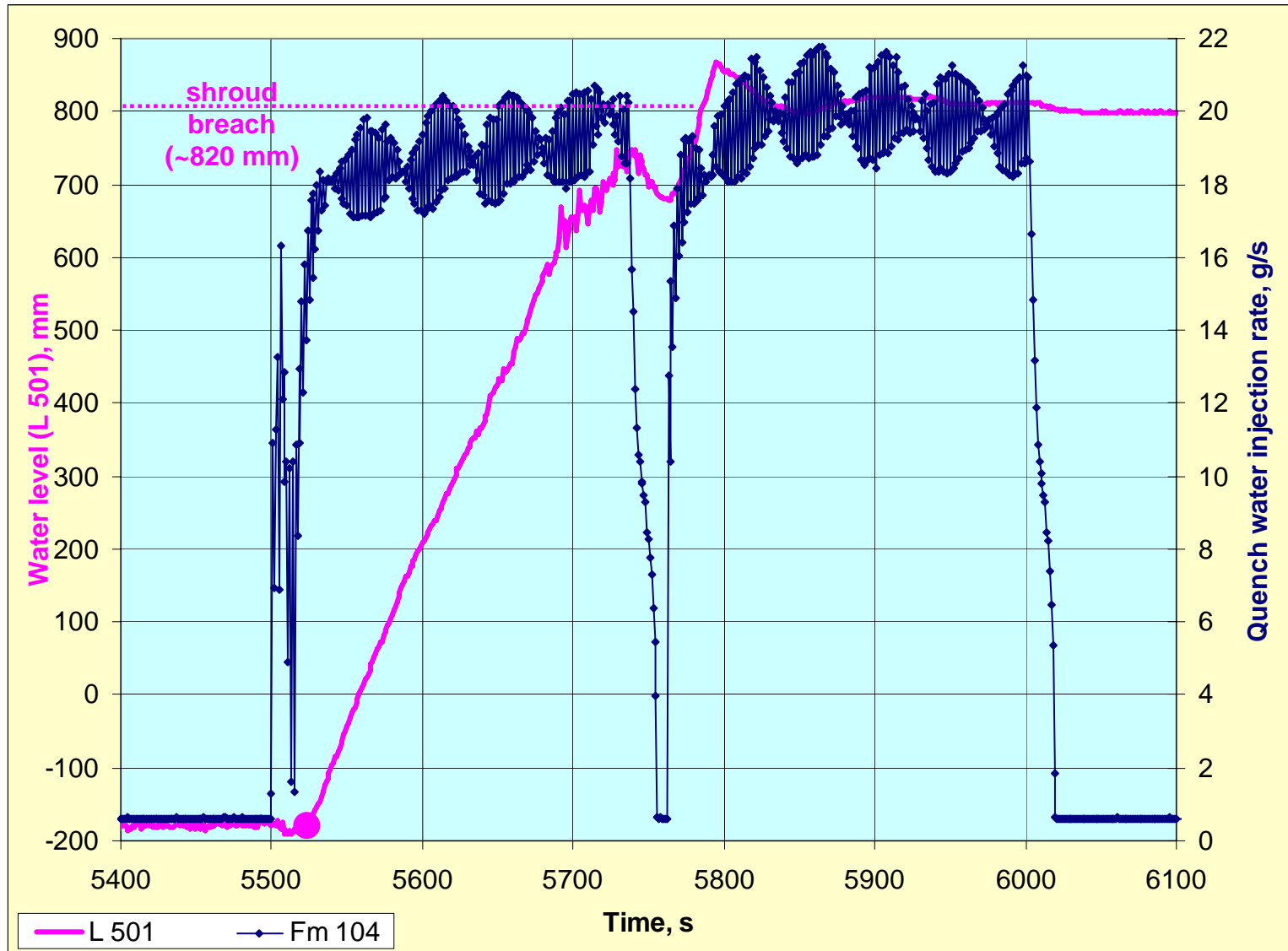


**QUENCH-11: appearance of the corner Zry-rod,
withdrawn from the bundle prior to the quench phase.
Thin, not spalled oxide layer. Thick β -Zry layer.**



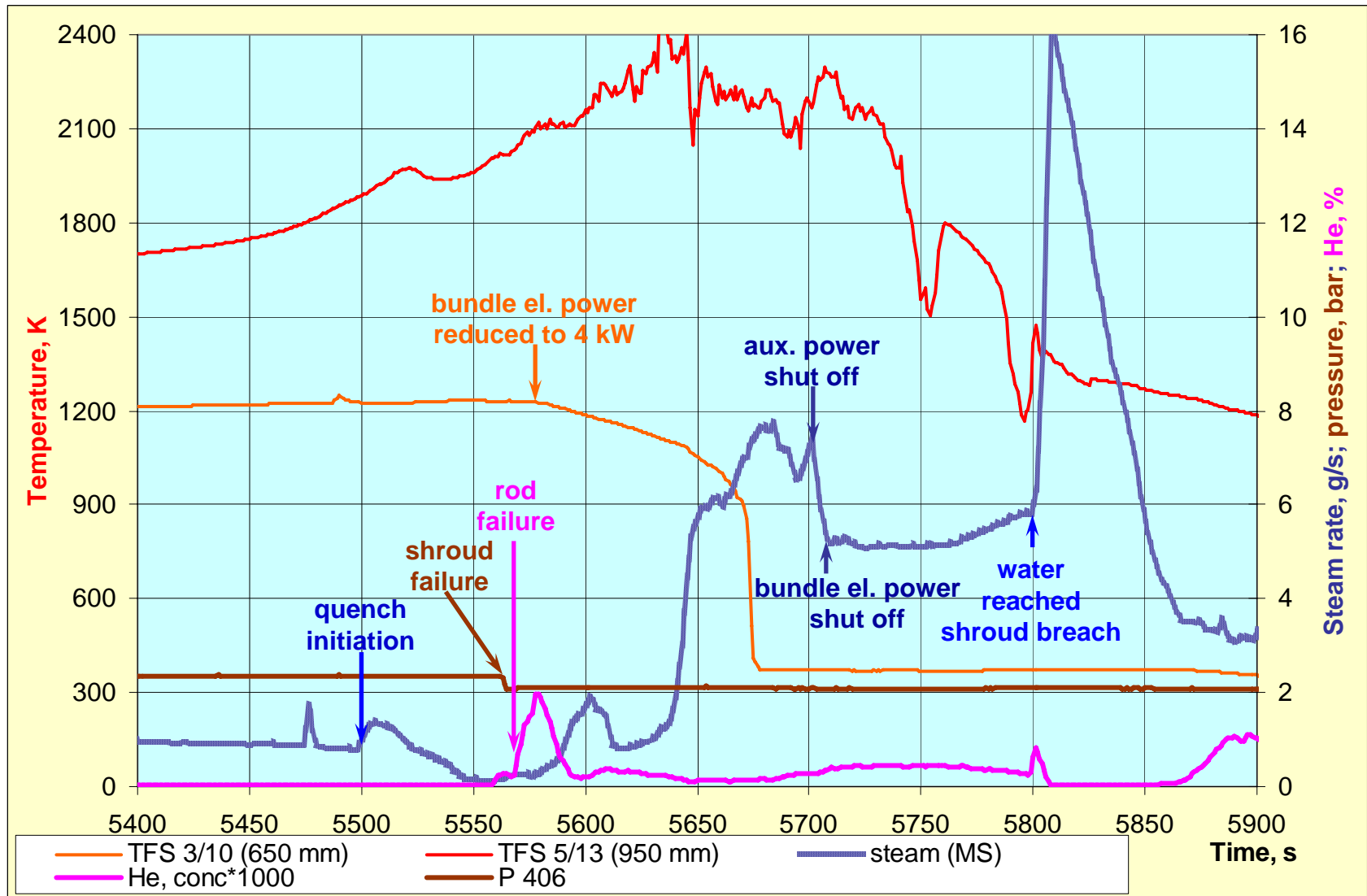


QUENCH-11, quench phase: slow flooding rate (18 – 20 g/s).
Water level increase rate: ~4.5 cm/s



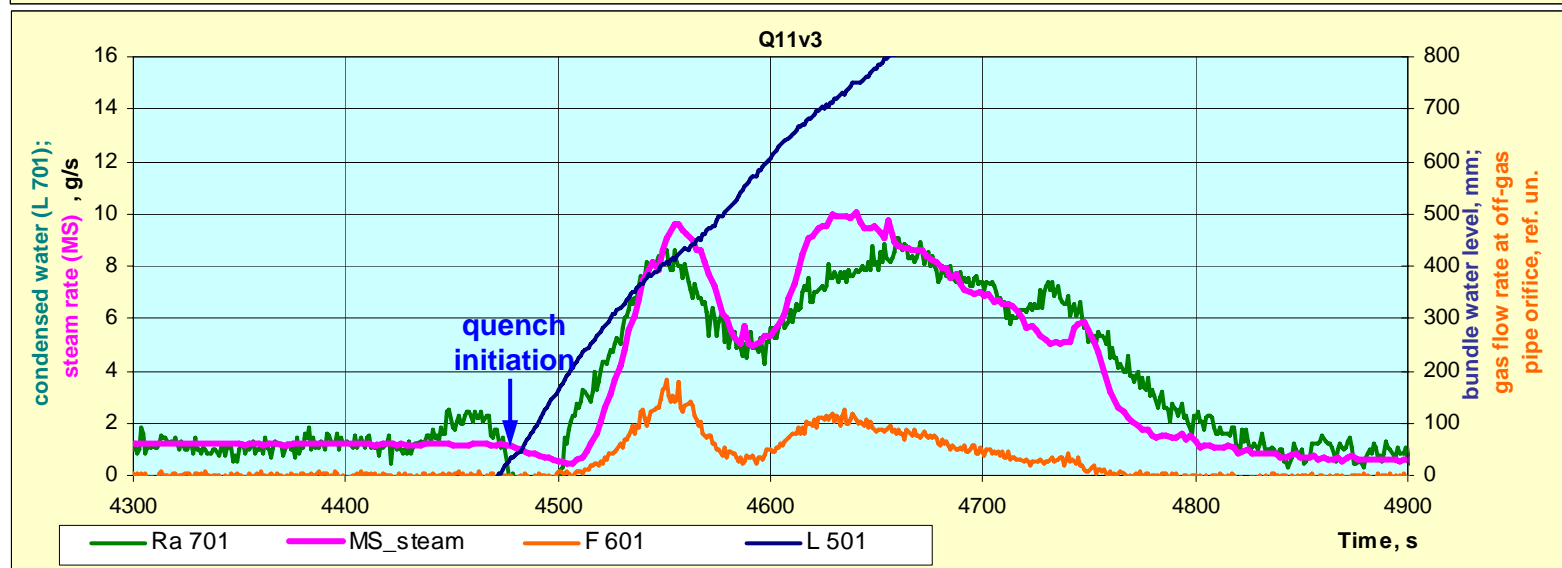
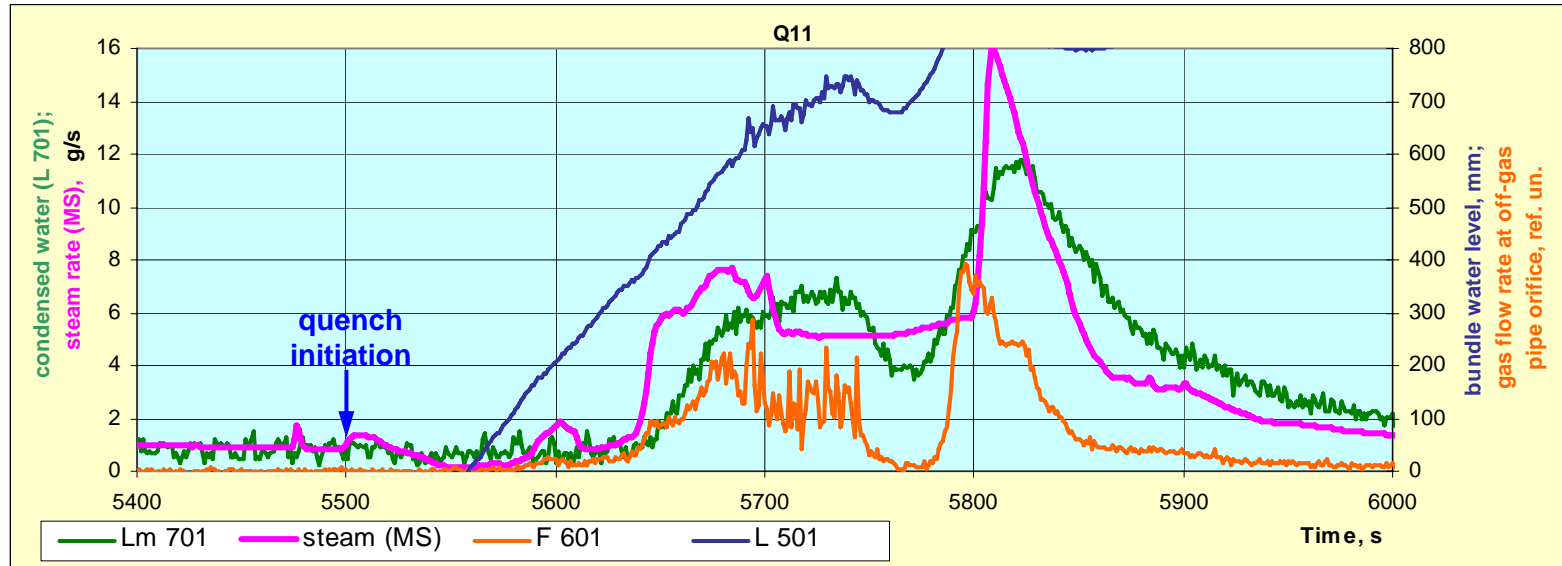


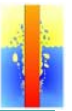
QUENCH-11, quench phase: sequence of events



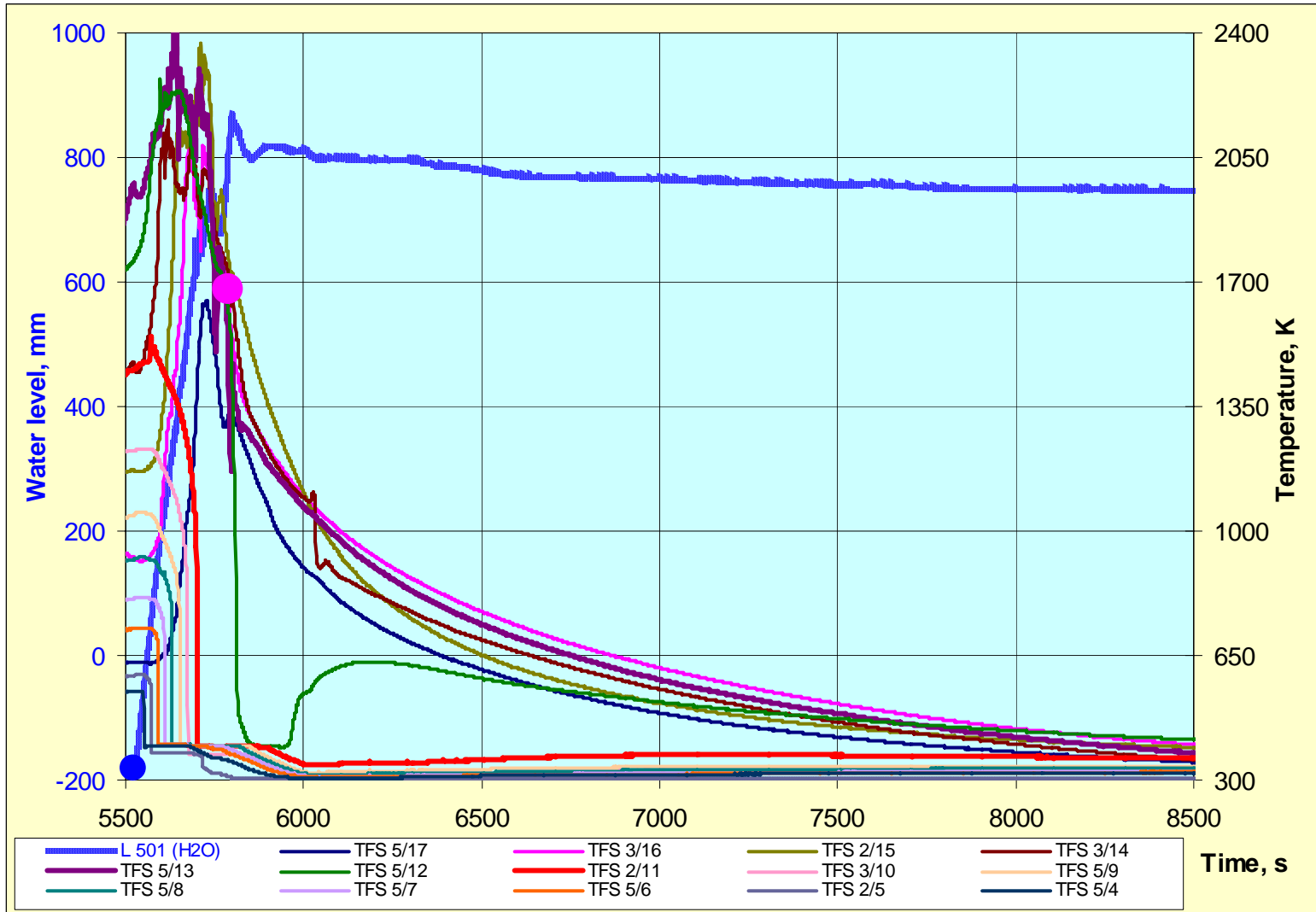


QUENCH-11, quench phase: different detection of steam production.
Comparison with pre-test Q11v3.



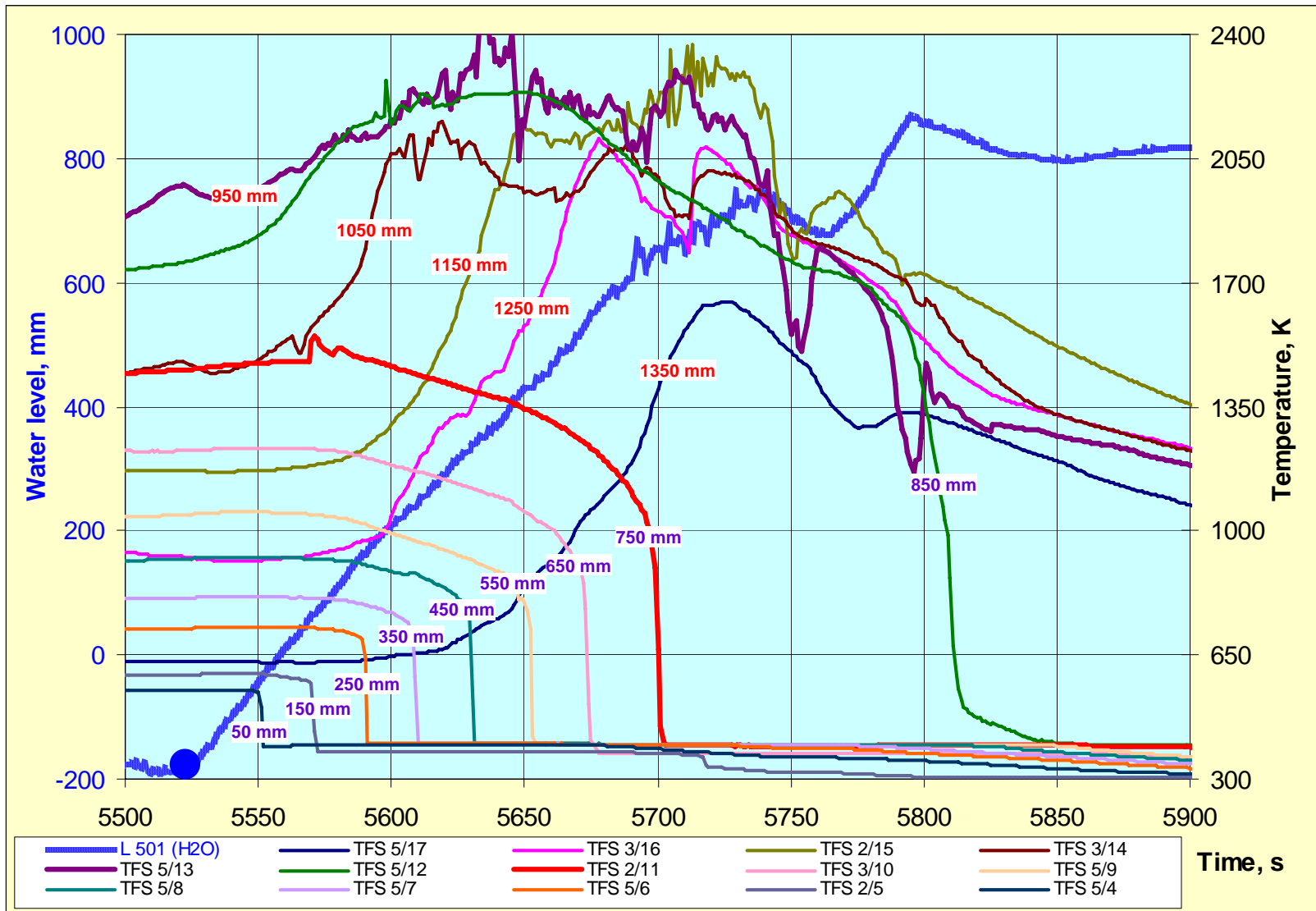


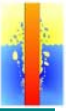
QUENCH-11, cooling phase: water reached the location of shroud breach (~850 mm);
bundle elevations 13 – 17 (950 mm – 1350 mm) cooled slowly during 3000 s
in decreased steam flow



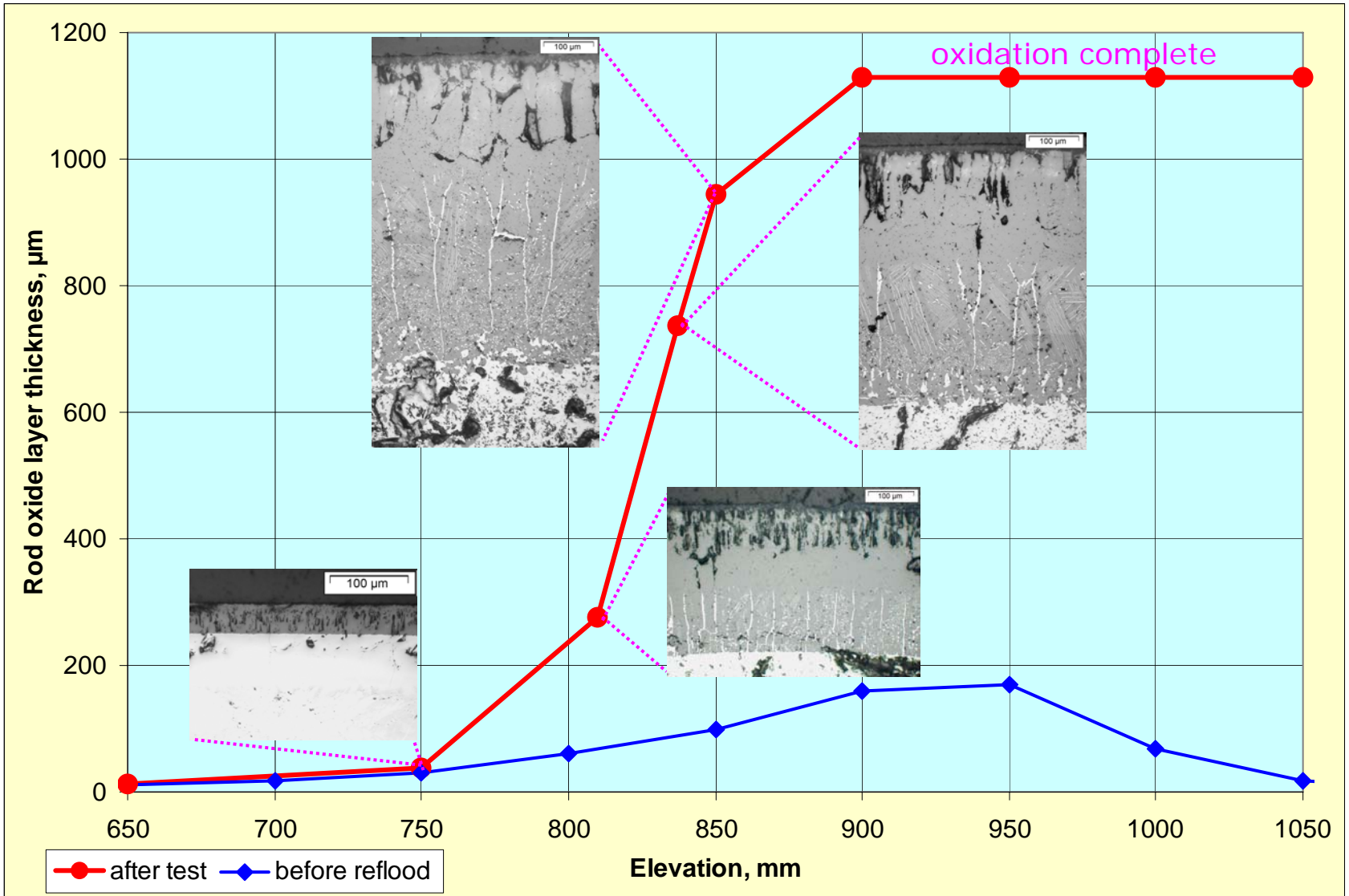


QUENCH-11, phase of slow reflood : accelerated TC reaction on the rising water surface due to two-phase region above the water surface. Escalation at elevations upper 950 mm.



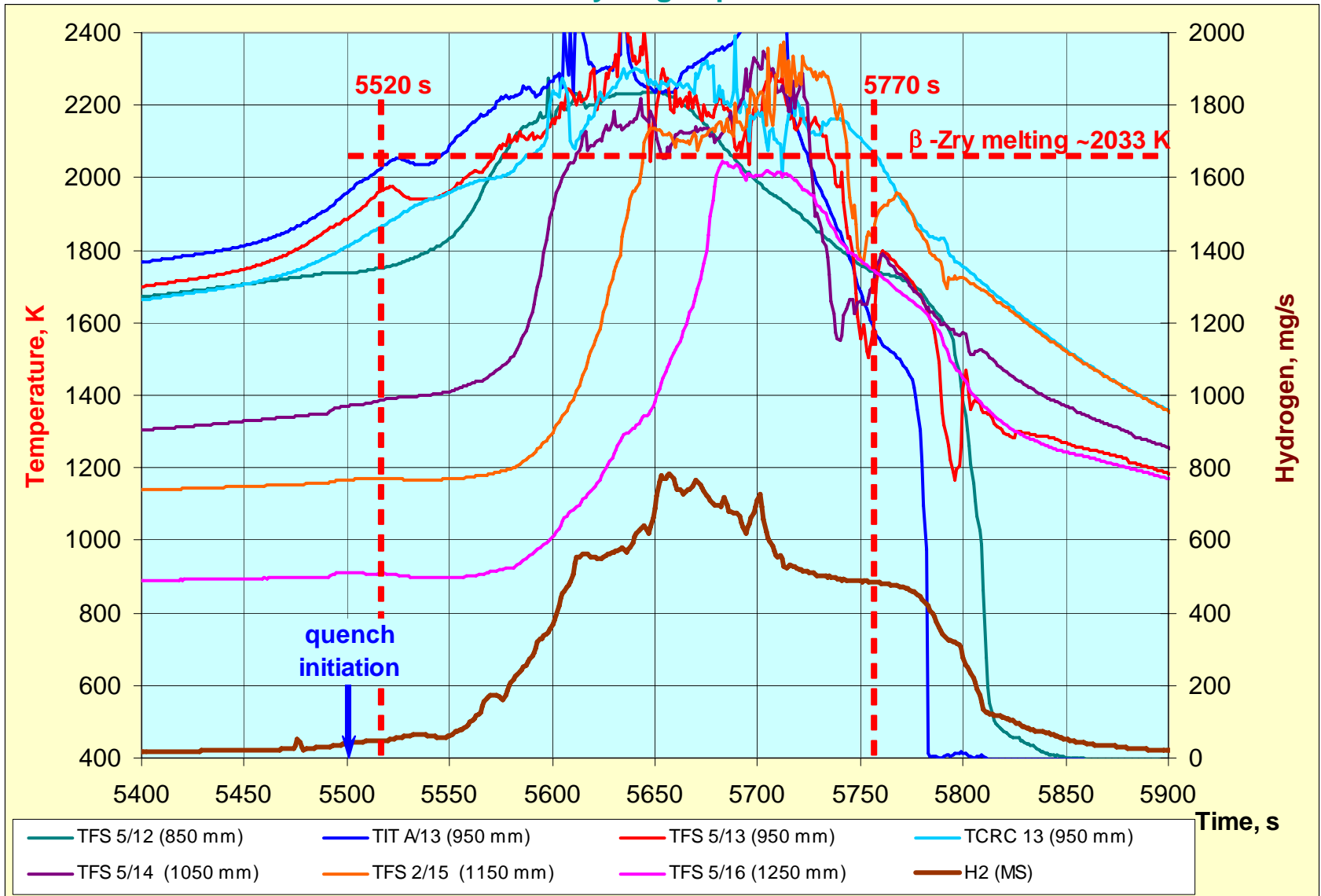


QUENCH-11, pos-test analysis: intensive growth of oxide layer during quench phase



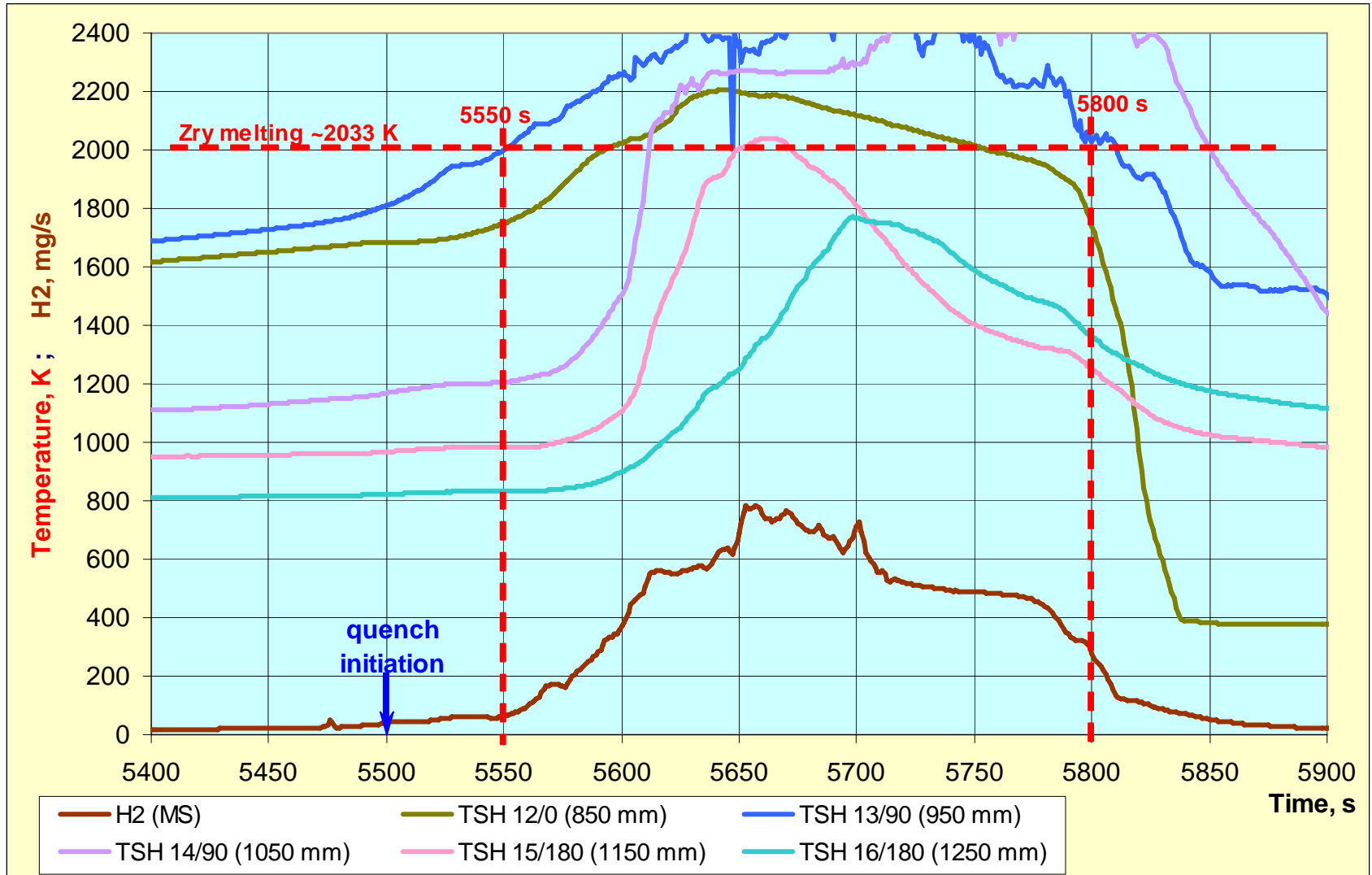


Q11, phase of slow reflow : bundle temperatures escalate above melting point of β -Zry.
Intensive hydrogen production.



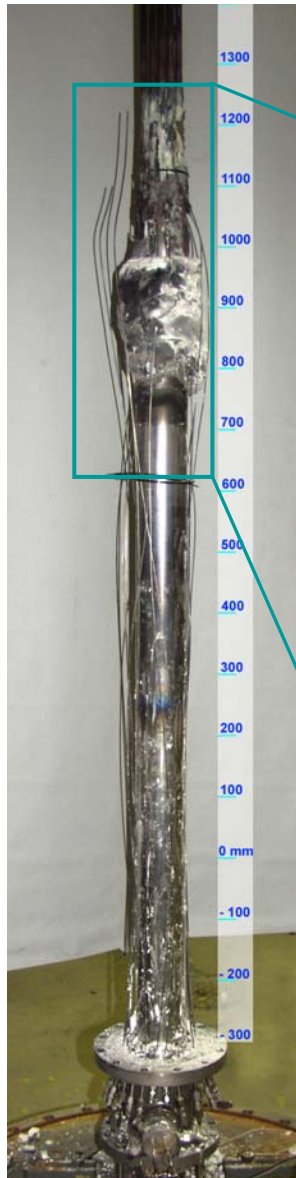


Q11, phase of slow reflood : shroud temperatures escalate above melting point of β -Zry.

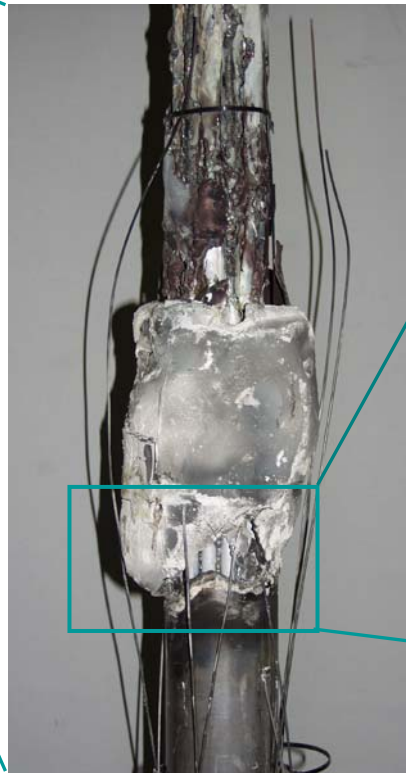




Q-11: intensive bundle damage above elevation of 800 mm

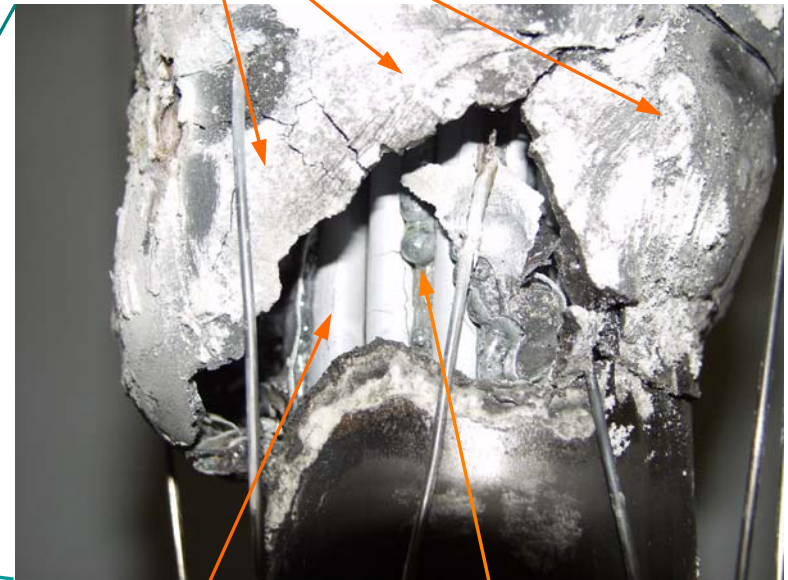


Position: 90°



Position: 270°

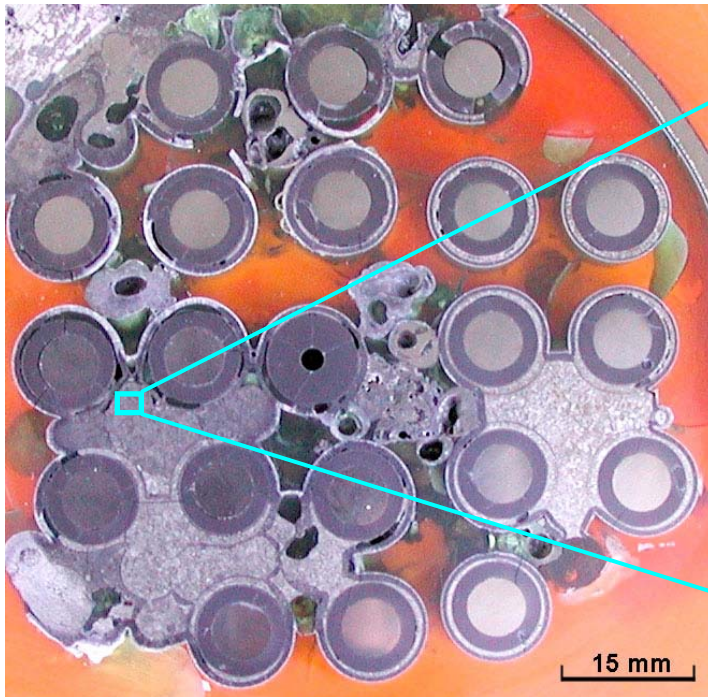
shrank thermal insulation, interacted with molten shroud



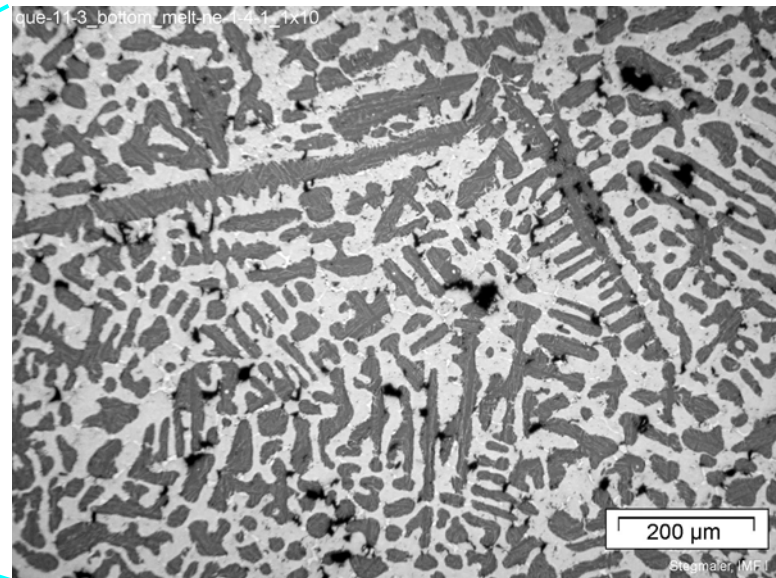
oxidised cladding

melt rivulets
between rods

Q-11: melt inside of the bundle at elevation 837 mm



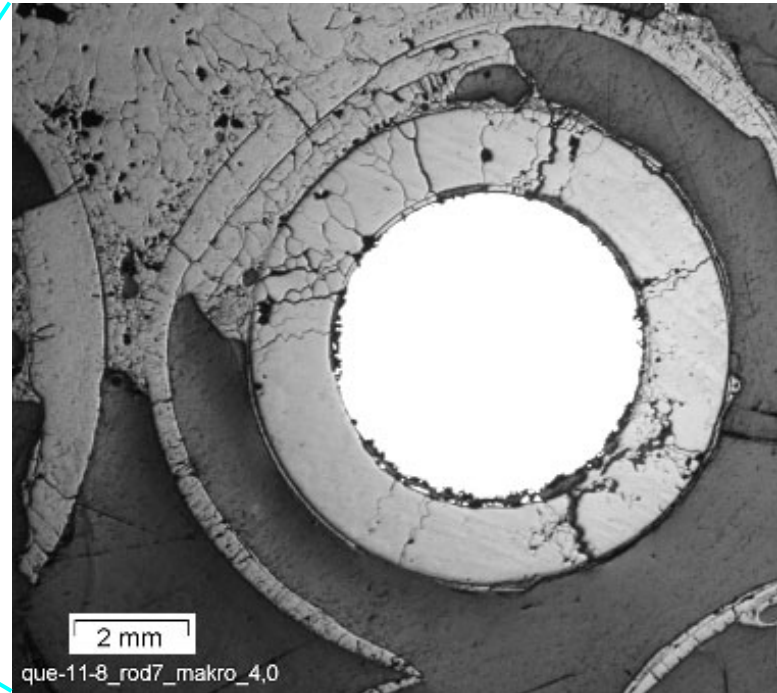
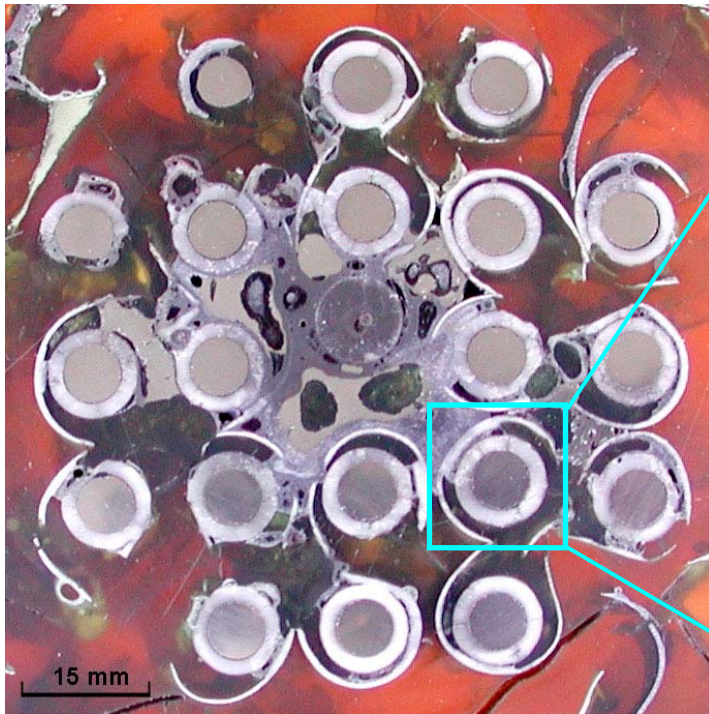
solidified melt between rods



**ZrO₂ dendrites: 54 % of area,
corresponding relationship Zr:O = 47.4:52.6 (at%),
i.e. the oxide precipitates start to develop
in the molten melt**



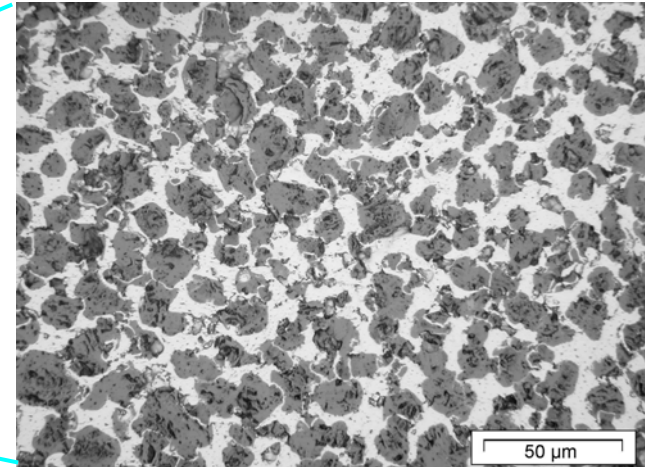
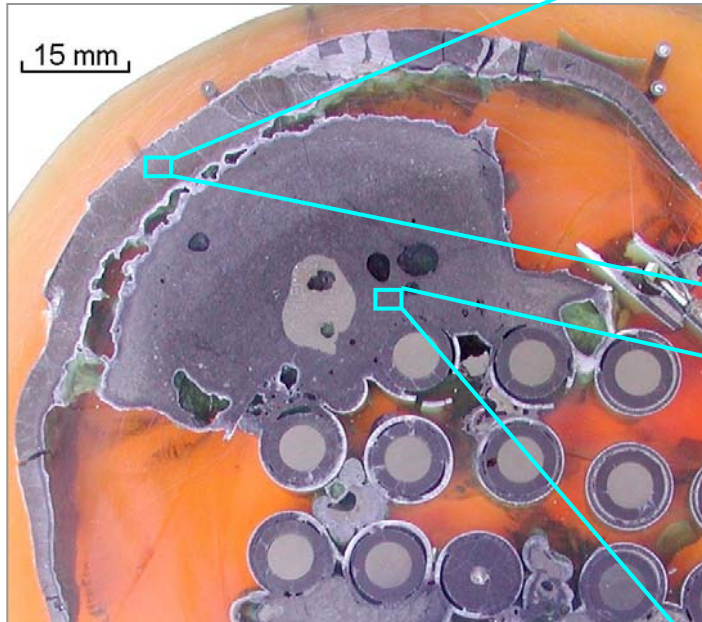
Q-11: melt inside of the bundle at elevation 1000 mm



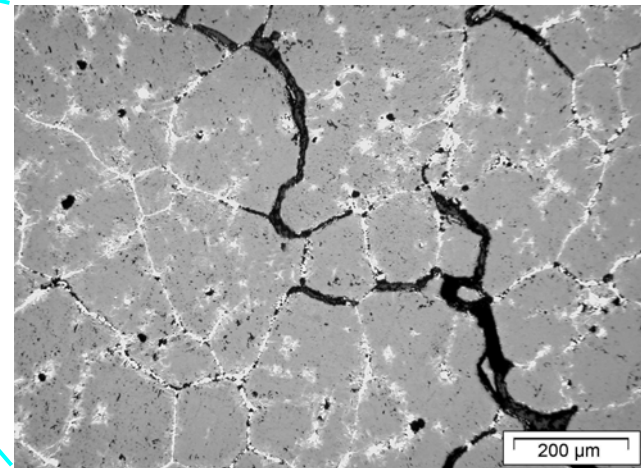
completely oxidised melt



QUENCH-11: shroud melt oxidation, elevation 850 mm



dissolution of fiber insulation by molten shroud



completely oxidised relocated melt



SUMMARY

- The QUENCH-11 test was performed in four stages: 1) Boil-off stage, 2) Stationery auxiliary water feeding at evaporation rate ~ 1.1 g/s and bundle temperature ramping from 873 K to 1773 K, 3) Temperature escalation to 2000 K, 4) Quench with a low flow rate of 18 g/s.
- The height of the two-phase region above collapsed water level was between 180 mm and 370 mm.
- The maximum oxide layer thickness before reflood was 170 μm (bundle elevation 950 mm).
- The first failure of a fuel rod simulator with simultaneous shroud failure were detected after 1 minute from quench initiation. The shroud failed at an elevation about 800 mm.
- The maximum of temperatures of 2383 K was reached in 2 minutes after quench initiation.
- Intensive melt formation and relocation was observed at elevations above 800 mm.
- The total generation of hydrogen was 141 g. During the reflood was produced 132 g hydrogen.